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CREATING EQUATION OF STATE OF CONDENSED SYSTEMS FROM DYNAMIC EXPERIMENTS

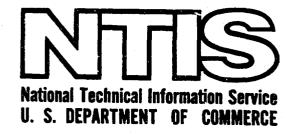
V. E. Fortov

Foreign Technology Division Wright-Patterson Air Force Base, Ohio

15 November 1974

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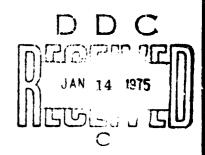


CREATING EQUATION OF STATE
OF CONDENSED SYSTEMS FROM DYNAMIC EXPERIMENTS

by

V. Ye. Fortov





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When written as ë in Rusian, transliterate as yë or ë.
The use of diacritical arks is preferred, but such marks may be omitted when expliency dictates.

FOLLOWING ARE THE CORRESPONDING RUSSIAN AND ENGLISH DESIGNATIONS OF THE TRIGONOMETRIC FUNCTIONS

Russian	English
sin	sin
008	COS
tg	ten
ctg	cot
50 C	80 C
COSC	CEC
sh	sinh
ch	cosh
th	tanh
cth	coth
sch	sech
csch	csch
arc sin	sin-l
erc cos	cos ⁻¹
arc tg	tan-l
arc ctg	cot ⁻¹
are sec	sec-l
arc comec	sin ⁻¹ cos ⁻¹ tan ⁻¹ cot ⁻¹ sec ⁻¹ csc ⁻
are sh	sinh-l
arc ch	sinh-l cosh-l
arc th	tenh-1
arc cth	coth-l
arc sch	sech-l
arc cach	csch-l
rot	A1171
lg	curl
- R	log

GREEK ALPHABET

Alpha	Α	α	•	Nıı	N	ν	
Beta	В	β		Xi	[2]	ξ	
Gamma	Γ	Υ		Omicron	0	0	
Delta	Δ	δ		Pi	Π	· IT	
Epsilon	E	ε	ŧ	Rho	P	ρ	
Zeta	Z	ζ		Sigma	Σ	σ	ς
Eta	H	η		Tau	T	τ	
Theta	Θ	θ	•	Upsilon	T	υ	
Iota	I	ι		Phil	Φ	φ	ф
Kappa	K	×	K	Chi	X	χ	
Lambda	٨	λ		Psi	Ψ	ψ	
Mu	M	μ		Omega	Ω	ω	

CREATING EQUATION OF STATE OF CONDENSED SYSTEMS FROM DYNAMIC EXPERIMENTS

V. Ye. Fortov Moscow

Successive theoretical calculation of the thermodynamic properties of a substance in the condensed state involves the quantum mechanics problem of many bodies when there exists a strong interaction among them. At the present time this cannot be achieved in a general form. In this situation experimental, primarily dynamic, research methods based on obtaining the necessary state by compression and irreversible heating of the medium at the front of a strong shock wave [1] acquire particular significance.

The characteristic feature of dynamic experiments is direct registration of only the mechanical parameters of shock compression - pressure (p), specific volume (V), and internal energy (E). To construct the complete equation of state from these data we must introduce model representations of the properties of the studied substance. Here the data of the experiment were used to determine the constants and functions contained in the equation of state; for certain terms purely theoretical expressions are

often used. The criterion of correctness for equations of state thus obtained is agreement between calculated and measured states of shock compression. Here a situation may arise in which various equations of state result in different values of the Grüneisen coefficient and temperature for the shock-compressed substance, even though the original experimental material was well described [2].

The thermodynamically complete equation of state, however, may be plotted from dynamic experiments without introducing limiting ideas concerning the properties and the nature of the studied medium [3, 4].

In dynamic experiments registration of the kinematic parameters of propagation of a shock discontinuity makes it possible, by using the general laws of conservation on the shock wave front, to determine the equation of state in a caloric form L=E(p, V) for the entire region of the pV plane accessible in the experiment [1]. The internal energy, however, does not represent thermodynamic potential with respect to the pV variable, and in order to plot the complete thermodynamics of the studied system we need the additional dependence T=T(p, V).

Proceeding from the first principle of thermodynamics and assuming that from the experiment the dependence E=E(p, V) is known, we can easily obtain [3]

$$\left[\rho + \left(\frac{\partial E}{\partial V}\right)_{\rho}\right] \cdot \frac{\partial T}{\partial \rho} - \left(\frac{\partial E}{\partial \rho}\right)_{V} \cdot \frac{\partial T}{\partial V} = T. \tag{1}$$

The solution to this linear heterogeneous differential equation with variable coefficients is the dependence T=T(p, V) which interests us. Equation (1) has a corresponding system of characteristic differential equations:

$$\frac{dp}{dV} = -\frac{n + \left(\frac{\partial E}{\partial V}\right)_p}{\left(\frac{\partial E}{\partial p}\right)_V};$$

$$\frac{dI}{dS'} = \frac{T}{\left(\frac{dS'}{dp}\right)_{S'}},$$

the first of which determines pressure, the second - temperature on the isentrope. Equations (1) or (2) and (3) are completed by boundary conditions: temperature must be given in the region where it can be experimentally determined. In the present calculations the temperature was assigned as a function of specific volume on the isobar of atmospheric pressure; the experimental data of V=V(T) with respect to the thermal expansion of the substance were used.

The caloric equation of state E=E(p, V) was constructed from experimental points E_i , p_i , V_i $_{i=1}^N$ chaintically arranged in the pV plane in the form of

$$E^{q}(p, V) = \sum_{k \in S_{q}} \sum_{i \in S_{k}} c_{ki} V^{k} p^{i}. \tag{4}$$

In (4) the coefficients e_{ki} are found by the method of least squares [4]. In determining coefficients e_{kl} the weight inversely proportional to registration error of the shock compression states was assumed by each experimental point.

The degree of the polynomial q in (4) was selected by analyting the residual sum of squares when the degree increased q+q+1. Here the statistical Fischer significance criterion [5] was used.

The equation of state in calculations of adiabatic flows.

The isentropes are determined by integrating differential equations (1) and (3); The shock adiabats are found by numerical solution to the Rankin-Hugonoit relationship:

$$\frac{1}{2}(p+p_0)(V_c-V) = E^{\phi}(p,V) - E_{\phi}(p_0,V_0). \tag{15}$$

where $\mathbb{E}^{\mathbf{q}}(\mathbf{p}, \mathbf{V})$ is taken in the form of (4).

The dependence tetween the accuracy of the obtained solution and error in the original data was determined by the Monte Carlo me had by simulating the probability structure of the measuring process on the electronic computer [4]. The computer reassembled possible combinations of random factors resulting in experimental arror and determined the effect of these factors on the solution to equations (2) and (3). The proposed method enabled a compressive estimate for the accuracy of the solution obtained for an given configuration of experimental points in the pV plane and the specific level of experimental errors.

an example we introduce the results for the equation of state for nickel. For this we used experimental data for dynamic for resistion of solid [6, 7, 8] and porous specimens of a given element. In addition the internal energy (according to [10]) was assigned at two points on the atmospheric pressure isobar. As the original data for system (2), (3) we use the results of examing the thermal expansion of nickel [11] at p=1 bar

Static analysis [4] showed that to describe the existing experimental data we must select the degree of the polynomial (4) q=3. Figure 1 shows the Hugonoit adiabats (Ni) plotted from the obtained equation of state. The difference between shock compression states calculated according to (4) and (5) and those which were measured lies within the limits of experimental error.

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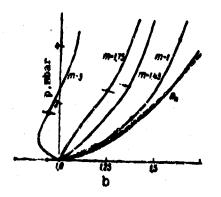


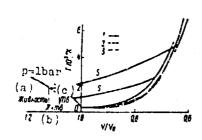
Figure 1. Hugonoit adiabats for mickel of different initial porosities $m = \frac{\rho_H}{\rho_0}$ (ρ_H density of crystal, ρ_0 density of original specimen); ρ_X - zero isentrope for equations (2) and (4); dashed line - zero isentrope for [2]; 0-[7]; V-[8]; Δ -[6]; Φ -p=1 bar).

An important characteristic of the substance used in all model theories for the equation of state is the "cold" compression curve $p_{\chi}(V)$ - the dependence of pressure on specific volume at $T=0^{\circ}K$. Existing methods for obtaining this curve from the results of the experiment involve introducing a large number of theoretical ideas about the properties of the studied substance. Assuming that the isotherm $T=0^{\circ}K$ coincides with the isentrope, the cold compression curve in this approach can be obtained by integrating equation (2) for $T_0=0^{\circ}K$. The elastic pressure curve thus plotted is shown in Fig. 1, where it is compared with $p_{\chi}(V)$ from [2].

It should be mentioned that, in contrast to existing theories, there was no preliminary division of the thermodynamic factors into "thermal" and "cold" components in the method of constructing an equation of state which is discussed here.

Temperature was calculated by combined integration of equations (2) and (3). For the initial value of the specific volume temperature was determined by means of the thermal expansion curve introduced into the computer (p=1 bar). With these initial conditions system (2), (3) was integrated up to the intersection of the isentrope with the shock adiabat in the pV plane of the solid substance. Figure 2 shows the results of determining temperature; here we also see for comparison the results of calculating temperatures on shock adiabats for solid nickel according to the Mie-Grüneisen theory [6] and in the

approximation of the theory of free volume [7].



Calculation for Figure 2. 1 - from temperature of nickel: equations (2), (3), $(\frac{1}{4})$; 2 study [6]; 3 - study [7]; s isentropes. (a) Liquid; (b) Liquid+sol-Key: id; (c) Solid.

The characteristic temperature "step" on the shock adiabat is the result of the melting of the substance at the front of the shock wave. The absence of detailed experimental data in the region of the melting curve resulted in a situation in which the melting curve coincided with the isentrope in this case; the real temperature "step" (according to [12]) is located

somewhere above that which is shown in Fig. 2.

The statistical analysis made by Monte Carlo method showed that if accuracy in the nature of the arrangement of the experimental points in the pV plane are considered the error in determining temperature on the Hugonoit adiabat for solid nickel is on the order of 5-8%, which is independently confirmed by comparison to temperature calculations for model theories of the equation state

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